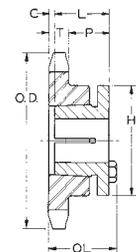


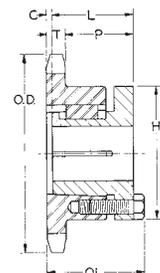
**SPROCKETS FOR No. 50.  $\frac{5}{8}$ " PITCH ANSI CHAIN**

**TABLE No. 1 STEEL SINGLE SPROCKETS WITH BROWNING SPLIT TAPER® BUSHINGS**

PART No.	BUSHING	BORE RANGE	DIAMETERS		No. TEETH	TYPE	DIMENSIONS						Wt. Less BUSHING
			OUTSIDE	PITCH			T NOM.	OL	L	P	C	H	
H50G11	G	$\frac{3}{8}$ - 1"	2.50"	2.219"	11	3	0.343"	1 $\frac{19}{32}$ "	1"	1 $\frac{3}{32}$ "	$\frac{7}{16}$ "	2"	0.5
H50G12	G	$\frac{3}{8}$ - 1	2.70	2.415	12	3	0.343	1 $\frac{19}{32}$	1	1 $\frac{3}{32}$	$\frac{7}{16}$	2	0.5
H50G13	G	$\frac{3}{8}$ - 1	2.91	2.612	13	3	0.343	1 $\frac{1}{4}$	1	$\frac{23}{32}$	$\frac{1}{16}$	2	0.5
H50H13	H	$\frac{3}{8}$ - 1 $\frac{1}{2}$	2.91	2.612	13	3	0.343	1 $\frac{23}{32}$	1 $\frac{1}{4}$	1 $\frac{5}{32}$	$\frac{1}{4}$	2 $\frac{1}{2}$	0.6
H50H14	H	$\frac{3}{8}$ - 1 $\frac{1}{2}$	3.11	2.809	14	3	0.343	1 $\frac{5}{8}$	1 $\frac{1}{4}$	1 $\frac{3}{32}$	$\frac{3}{16}$	2 $\frac{1}{2}$	0.6
H50H15	H	$\frac{3}{8}$ - 1 $\frac{1}{2}$	3.32	3.006	15	3	0.343	1 $\frac{1}{2}$	1 $\frac{1}{4}$	$\frac{31}{32}$	$\frac{1}{16}$	2 $\frac{1}{2}$	0.8
H50P15	P1	$\frac{1}{2}$ - 1 $\frac{3}{4}$	3.32	3.006	15	4	0.343	2 $\frac{3}{16}$	1 $\frac{15}{16}$	1 $\frac{19}{32}$	0	3	1.1
H50H16	H	$\frac{3}{8}$ - 1 $\frac{1}{2}$	3.52	3.204	16	3	0.343	1 $\frac{1}{2}$	1 $\frac{1}{4}$	$\frac{31}{32}$	$\frac{1}{16}$	2 $\frac{1}{2}$	0.9
H50P16	P1	$\frac{1}{2}$ - 1 $\frac{3}{4}$	3.52	3.204	16	4	0.343	2 $\frac{3}{16}$	1 $\frac{15}{16}$	1 $\frac{19}{32}$	0	3	1.3
H50H17	H	$\frac{3}{8}$ - 1 $\frac{1}{2}$	3.72	3.401	17	3	0.343	1 $\frac{1}{2}$	1 $\frac{1}{4}$	$\frac{31}{32}$	$\frac{1}{16}$	2 $\frac{1}{2}$	1.0
H50P17	P1	$\frac{1}{2}$ - 1 $\frac{3}{4}$	3.72	3.401	17	4	0.343	2 $\frac{3}{16}$	1 $\frac{15}{16}$	1 $\frac{19}{32}$	0	3	1.4
H50H18	H	$\frac{3}{8}$ - 1 $\frac{1}{2}$	3.92	3.599	18	3	0.343	1 $\frac{1}{2}$	1 $\frac{1}{4}$	$\frac{31}{32}$	$\frac{1}{16}$	2 $\frac{1}{2}$	1.0
H50P18	P1	$\frac{1}{2}$ - 1 $\frac{3}{4}$	3.92	3.599	18	4	0.343	2 $\frac{3}{16}$	1 $\frac{15}{16}$	1 $\frac{19}{32}$	0	3	1.6
H50H19	H	$\frac{3}{8}$ - 1 $\frac{1}{2}$	4.12	3.797	19	3	0.343	1 $\frac{1}{2}$	1 $\frac{1}{4}$	$\frac{31}{32}$	$\frac{1}{16}$	2 $\frac{1}{2}$	1.1
H50P19	P1	$\frac{1}{2}$ - 1 $\frac{3}{4}$	4.12	3.797	19	4	0.343	2 $\frac{3}{16}$	1 $\frac{15}{16}$	1 $\frac{19}{32}$	0	3	1.8
H50H20	H	$\frac{3}{8}$ - 1 $\frac{1}{2}$	4.32	3.995	20	3	0.343	1 $\frac{1}{2}$	1 $\frac{1}{4}$	$\frac{31}{32}$	$\frac{1}{16}$	2 $\frac{1}{2}$	1.5
H50P20	P1	$\frac{1}{2}$ - 1 $\frac{3}{4}$	4.32	3.995	20	4	0.343	2 $\frac{3}{16}$	1 $\frac{15}{16}$	1 $\frac{19}{32}$	0	3	2.0
H50H21	H	$\frac{3}{8}$ - 1 $\frac{1}{2}$	4.52	4.194	21	3	0.343	1 $\frac{1}{2}$	1 $\frac{1}{4}$	$\frac{31}{32}$	$\frac{1}{16}$	2 $\frac{1}{2}$	1.4
H50P21	P1	$\frac{1}{2}$ - 1 $\frac{3}{4}$	4.52	4.194	21	4	0.343	2 $\frac{3}{16}$	1 $\frac{15}{16}$	1 $\frac{19}{32}$	0	3	2.1
H50H22	H	$\frac{3}{8}$ - 1 $\frac{1}{2}$	4.72	4.392	22	3	0.343	1 $\frac{1}{2}$	1 $\frac{1}{4}$	$\frac{31}{32}$	$\frac{1}{16}$	2 $\frac{1}{2}$	1.5
H50P22	P1	$\frac{1}{2}$ - 1 $\frac{3}{4}$	4.70	4.392	22	4	0.343	2 $\frac{3}{16}$	1 $\frac{15}{16}$	1 $\frac{19}{32}$	0	3	2.3
H50H23	H	$\frac{3}{8}$ - 1 $\frac{1}{2}$	4.92	4.590	23	3	0.343	1 $\frac{1}{2}$	1 $\frac{1}{4}$	$\frac{31}{32}$	$\frac{1}{16}$	2 $\frac{1}{2}$	1.7
H50P23	P1	$\frac{1}{2}$ - 1 $\frac{3}{4}$	4.92	4.590	23	4	0.343	2 $\frac{3}{16}$	1 $\frac{15}{16}$	1 $\frac{19}{32}$	0	3	2.4
H50Q23	Q1	$\frac{3}{4}$ - 2 $\frac{11}{16}$	4.92	4.590	23	4	0.343	2 $\frac{53}{64}$	2 $\frac{1}{2}$	2 $\frac{1}{4}$	$\frac{3}{32}$	4 $\frac{1}{8}$	3.4
H50H24	H	$\frac{3}{8}$ - 1 $\frac{1}{2}$	5.12	4.788	24	3	0.343	1 $\frac{1}{2}$	1 $\frac{1}{4}$	$\frac{31}{32}$	$\frac{1}{16}$	2 $\frac{1}{2}$	1.8
H50P24	P1	$\frac{1}{2}$ - 1 $\frac{3}{4}$	5.12	4.788	24	4	0.343	2 $\frac{3}{16}$	1 $\frac{15}{16}$	1 $\frac{19}{32}$	0	3	2.5
H50Q24	Q1	$\frac{3}{4}$ - 2 $\frac{11}{16}$	5.12	4.788	24	4	0.343	2 $\frac{53}{64}$	2 $\frac{1}{2}$	2 $\frac{1}{4}$	$\frac{3}{32}$	4 $\frac{1}{8}$	3.4
H50H25	H	$\frac{3}{8}$ - 1 $\frac{1}{2}$	5.32	4.987	25	3	0.343	1 $\frac{1}{2}$	1 $\frac{1}{4}$	$\frac{31}{32}$	$\frac{1}{16}$	2 $\frac{1}{2}$	1.9
H50P25	P1	$\frac{1}{2}$ - 1 $\frac{3}{4}$	5.32	4.987	25	4	0.343	2 $\frac{3}{16}$	1 $\frac{15}{16}$	1 $\frac{19}{32}$	0	3	2.6
H50Q25	Q1	$\frac{3}{4}$ - 2 $\frac{11}{16}$	5.32	4.987	25	4	0.343	2 $\frac{53}{64}$	2 $\frac{1}{2}$	2 $\frac{1}{4}$	$\frac{3}{32}$	4 $\frac{1}{8}$	3.7
H50H26	H	$\frac{3}{8}$ - 1 $\frac{1}{2}$	5.52	5.185	26	3	0.343	1 $\frac{1}{2}$	1 $\frac{1}{4}$	$\frac{31}{32}$	$\frac{1}{16}$	2 $\frac{1}{2}$	2.0
H50P26	P1	$\frac{1}{2}$ - 1 $\frac{3}{4}$	5.52	5.185	26	4	0.343	2 $\frac{3}{16}$	1 $\frac{15}{16}$	1 $\frac{19}{32}$	0	3	2.9

**Hardened Teeth**


Type 3



Type 4

Where two sprockets with the same number of teeth but different bushings are offered, we suggest using the sprocket bushing for heavier service drives.

**STANDARD KEYSEATS**
**TABLE No. 2**

BORE RANGE	KEYSEAT
$\frac{3}{8}$ " - $\frac{7}{16}$ "	None
$\frac{1}{2}$ - $\frac{9}{16}$	$\frac{1}{8}$ " X $\frac{1}{16}$ "
$\frac{5}{8}$ - $\frac{7}{8}$	$\frac{3}{16}$ X $\frac{3}{32}$
$\frac{15}{16}$ - 1 $\frac{1}{4}$	$\frac{1}{4}$ X $\frac{1}{8}$
1 $\frac{5}{16}$ - 1 $\frac{3}{8}$	$\frac{5}{16}$ X $\frac{5}{32}$
1 $\frac{7}{16}$ - 1 $\frac{3}{4}$	$\frac{3}{8}$ X $\frac{3}{16}$
1 $\frac{13}{16}$ - 2 $\frac{1}{4}$	$\frac{1}{2}$ X $\frac{1}{4}$
2 $\frac{5}{16}$ - 2 $\frac{3}{4}$	$\frac{5}{8}$ X $\frac{5}{16}$
2 $\frac{13}{16}$ - 3 $\frac{1}{4}$	$\frac{3}{4}$ X $\frac{3}{8}$

 1  $\frac{3}{8}$ " Bore Bushings also available with  $\frac{3}{8}$ " x  $\frac{3}{16}$ " Keyseat.
